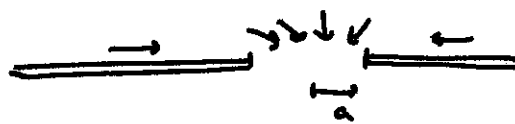


# Physics 211 - Final Exam

## Solutions

1.) a) We want to find  $\vec{v} = \vec{\nabla}\phi$  with  $\nabla^2\phi = 0$   
with the boundary condition



$V_1 = -V$  in the hole only.

The analogous electrostatics problem is



charge = 0

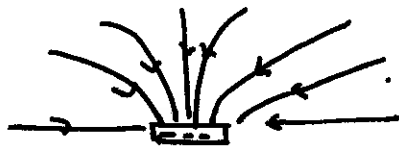
↑ charge density = constant

such that

$$\int_{|r|=a} d^2s \hat{n} \cdot \vec{E} = -\pi a^2 V$$

so

$\vec{E}$  or  $\vec{v}$  is the field of this charge distribution

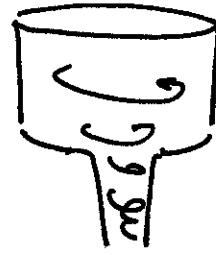


for  $|r| \gg a$  this is a monopole

$$\vec{v} = -\frac{V}{2} \frac{a^2}{r^2} \hat{r}$$



b) If  $\eta = 0$ , the only forces on a fluid element are pressure and gravity. Both are in the  $(r, z)$  plane. A torque requires a force  $\parallel \hat{\phi}$ .



Then  $\Delta L_z = \rho r v_\phi \Delta \text{Vol}$  remains fixed

$$v_\phi \sim \frac{1}{r} \quad \text{or} \quad v_\phi = V_0 \frac{a}{r}$$

The vorticity is

$$\vec{\omega} = \nabla \times \vec{v} \approx \hat{z} \frac{1}{r} \frac{\partial}{\partial r} (r v_\phi) = 0$$

But actually

$$\int d\ell \cdot \vec{\omega} \cdot \hat{n} = \int d\ell \cdot \vec{v} = 2\pi V_0 a$$



so  $\vec{\omega}$  is nonzero just at  $r=0$ :  $\vec{\omega} = \hat{z} 2\pi a V_0 \delta^{(2)}(x_\perp)$   
however, this is not relevant; see (c)

c.) From Bernoulli's theorem

$$\frac{P}{\rho} + \frac{1}{2} v^2 + gz = 0$$

at the surface,  $P = P_0$  atmospheric pressure. So

$$z = -\frac{1}{2g} v^2$$

or

$$z = - \frac{1}{2g} \frac{(V_0 a)^2}{r^2}$$



d.) In a rotating coordinate system, we add in the Coriolis force

$$e \frac{\partial \vec{v}}{\partial t} = -2\rho \vec{\Omega} \times \vec{v}$$

so, from above, if  $\vec{\Omega} \parallel \hat{z}$



on the surface of the earth, in the northern hemisphere, we have effectively  $\vec{\Omega} = +\hat{z} \left( \frac{2\pi}{\text{day}} \right) \cdot \cos \Theta$

The swirl is in the positive (counterclockwise) direction seen from above.

The effect is very weak  $\Omega \cdot (\text{char time}) \sim \frac{\text{sec}}{\text{day}} \sim 10^{-5}$

e.) In cylindrical coordinates, the  $\phi$  component of the N-S equation is

$$\frac{\partial v_\phi}{\partial t} + \vec{v} \cdot \vec{\nabla} v_\phi + \frac{v_r v_\phi}{r} = -\frac{1}{\rho} \frac{1}{r} \frac{\partial p}{\partial \phi} + \nu (\nabla^2 \vec{v})_\phi$$

In this setup  $v_r = 0$      $p = \text{fnctn of } r, z \text{ only}$      $\frac{\partial}{\partial \phi} p = 0$   
 $v_\phi = \text{fnctn of } r, z \text{ only}$      $\frac{\partial}{\partial \phi} v_\phi = 0$

so

$$\frac{\partial v_\phi}{\partial t} = \nu (\nabla^2 \vec{v})_\phi$$

for a thin boundary layer near  $r=a$      $\delta \ll a$

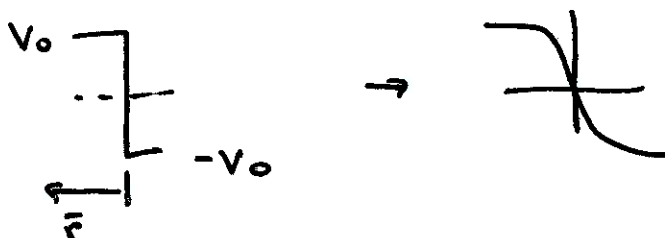
$$\frac{\partial v_\phi}{\partial t} = \nu \frac{d^2}{d\bar{r}^2} v_\phi \quad \bar{r} = a - r$$

The boundary conditions are:  $v_\phi = V_0$  at  $t=0, \bar{r} \rightarrow 0$

$$v_\phi = 0 \quad \text{at } \bar{r} = 0$$

$$v_\phi \rightarrow V_0 \quad \text{as } \bar{r} \rightarrow \infty$$

We can solve this by "method of images" for a diffusion problem



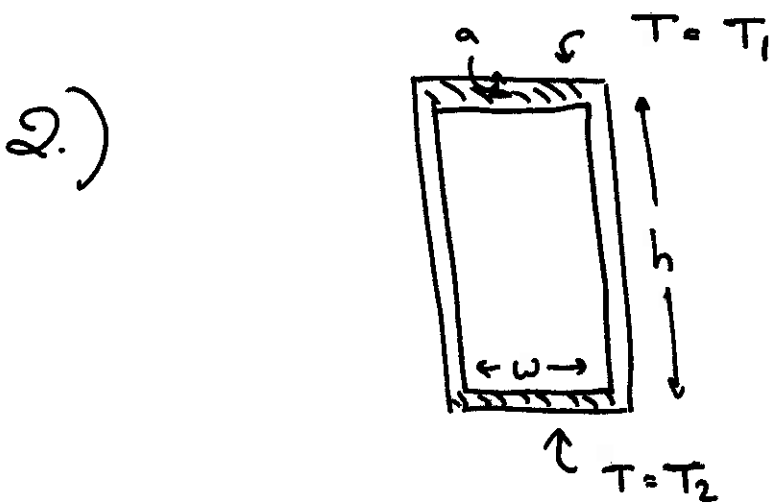
we discussed this diffusion problem in class. The solution is

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$$V_\phi = V_0 \operatorname{erf}\left(\frac{\bar{r}}{\sqrt{4\nu t}}\right) = \frac{2V_0}{\sqrt{\pi}} \int_0^{\bar{r}/\sqrt{4\nu t}} d\omega e^{-\omega^2}$$

In particular

$$\delta = \sqrt{4\nu t}$$



a) Poiseuille flow in the pipe gives a velocity distribution

$$v(r) = V_c \left(1 - \frac{r^2}{a^2}\right)$$

The force/area on the fluid is

$$\eta \left. \frac{\partial v}{\partial r} \right|_{r=a} = 2\eta \frac{V_c}{a}$$

$$\text{The force/length} = 2\eta \frac{V_c}{a} \cdot 2\pi a = 4\pi \eta V_c$$

The velocity averaged over the cross section is

$$\begin{aligned} V \cdot \pi a^2 &= \int_0^a dr r 2\pi V_c (1 - r^2/a^2) \\ &= 2\pi V_c \left( \frac{1}{2} - \frac{1}{4} \right) = \frac{1}{2} a^2 V_c \end{aligned}$$

so

$$V = \frac{1}{2} V_c$$

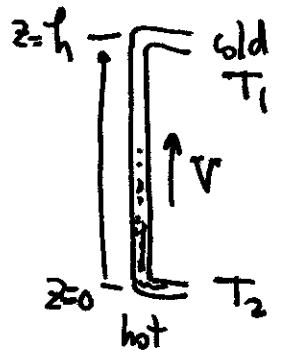
The equation of motion is

$$\pi a^2 \rho \cdot l \nu h \cdot \frac{\partial V}{\partial t} = -4\pi \eta V_c l = -8\pi \eta V \cdot l$$

$$\frac{\partial V}{\partial t} = -\frac{8\nu}{a^2} V$$

b.) In the vertical pipes,  $T$  obeys

$$\frac{\partial T}{\partial t} + \frac{2V}{V_c} \frac{\partial T}{\partial z} = \chi \frac{\partial^2}{\partial z^2} T$$



For  $V=0$ , the steady state is

$$\frac{\partial^2}{\partial z^2} T = 0 \Rightarrow T = T_2 - \Delta T \frac{z}{h}$$

For  $V > 0$ , the steady state is the solution of

$$2V \frac{dT}{dz} = \chi \frac{d^2}{dz^2} T$$

$$T = a + b \exp\left[\frac{2Vz}{\lambda}\right]$$

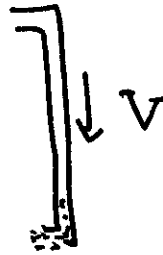
We must have  $T = T_2$  at  $z = 0$   $T = T_2 - \Delta T$  at  $z = h$

so

$$T = T_2 - \Delta T \left( \frac{\exp\left[\frac{2Vz}{\lambda}\right] - 1}{\exp\left[\frac{2Vh}{\lambda}\right] - 1} \right)$$

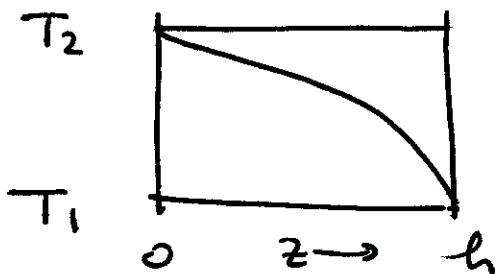
In the other pipe:

the positive direction for  $V$   
is down, so we send  
 $V \rightarrow -V$

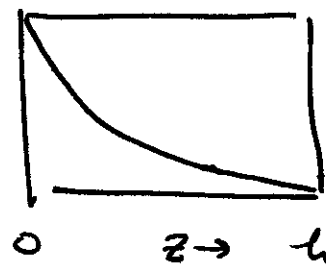


$$T = T_2 - \Delta T \left( \frac{1 - \exp\left[-\frac{2Vz}{\lambda}\right]}{1 - \exp\left[-\frac{2Vh}{\lambda}\right]} \right)$$

going up:



going down:



c.) In the Boussinesq approximation, the buoyancy force per unit volume is

$$\rho \alpha T g \quad \text{upward}$$

the force per unit length is

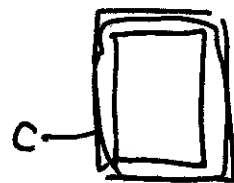
$$F/l = \pi a^2 \cdot \rho g \alpha T$$

To feel more comfortable about this, note that if  $T$  were constant there would be no net force on the fluid.

Note also that pressure exerts no net force on the fluid,

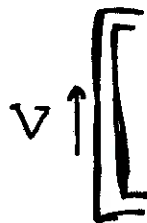
since

$$\oint_C dx \cdot \nabla p = 0$$



Now, the upward force on the left is

$$\begin{aligned} & \pi a^2 \rho g \alpha \int_0^h dz T(z) \\ & = \pi a^2 \rho g \alpha \left[ T_2 h - \Delta T \cdot \frac{\left(\frac{\chi}{2V}\right) (e^{\frac{2V}{\chi}} - 1) - h}{e^{\frac{2V}{\chi}} - 1} \right] \\ & = \pi a^2 \rho g \alpha \left[ T_2 h - \Delta T \left[ \frac{\chi}{2V} - \frac{h}{e^{\frac{2V}{\chi}} - 1} \right] \right] \end{aligned}$$



now

$$\begin{aligned}
 \frac{\lambda}{2V} - \frac{h}{e^{2Vh/\lambda} - 1} &= \frac{\lambda}{2V} - \frac{h}{\left(\frac{2Vh}{\lambda}\right) + \frac{1}{2}\left(\frac{2Vh}{\lambda}\right)^2 + \frac{1}{3!}\left(\frac{2Vh}{\lambda}\right)^3 + \dots} \\
 &= \frac{\lambda}{2V} \left[ 1 - \frac{1}{1 + \frac{1}{2}\left(\frac{2Vh}{\lambda}\right) + \frac{1}{6}\left(\frac{2Vh}{\lambda}\right)^2 + \dots} \right] \\
 &= \frac{\lambda}{2V} \left[ 1 - \left(1 - \frac{1}{2}\left(\frac{2Vh}{\lambda}\right) + \frac{1}{4}\left(\frac{2Vh}{\lambda}\right)^2 - \frac{1}{6}\left(\frac{2Vh}{\lambda}\right)^3 + \dots\right) \right] \\
 &= \frac{1}{2}h - \frac{1}{6}\frac{Vh^2}{\lambda} + \dots
 \end{aligned}$$

so the upward force on the left is

$$\pi a^2 \rho g \alpha \left[ (T_2 - \frac{1}{2} \Delta T) h + \frac{\Delta T}{6} \frac{V}{\lambda} h^2 + \dots \right]$$

The net force in the direction of  $V$  is (Left-Right)

$$\pi a^2 \rho g \alpha \frac{\Delta T}{3} \frac{V}{\lambda} h^2$$

To add this to the equation on p. 6, note that this would come in the form:

$$\underbrace{\pi a^2 \rho (2h + 2w)}_{\text{total mass}} \frac{dV}{dt} = \underbrace{\pi a^2 \rho g \alpha \frac{\Delta T}{3} \frac{V}{\lambda} h^2}_{\text{net force}}$$

$$\text{so } \frac{dV}{dt} = + BV \quad B = \frac{g \alpha \Delta T}{6\lambda} \frac{h^2}{h+w}$$

d.) The complete equation is

$$\frac{dV}{dt} = -\frac{8V}{a^2} V + \frac{g\alpha}{6X} \frac{\Delta T}{h+w} V + \dots$$

so  $V$  decreases exponentially when  $\Delta T$  is small but increases exponentially when

$$\Delta T > \frac{48\nu}{a^2} \frac{\chi}{g\alpha} \frac{(h+w)}{h^2}$$

The sign of  $V$  is chosen randomly. This is spontaneous symmetry breaking.

e.) The full equation for  $V$  is

$$\frac{dV}{dt} = -\frac{8V}{a^2} V + \frac{\pi a^2 g \rho \alpha}{\pi a^2 \rho (2h+2w)} f$$

$$\begin{aligned} \text{where } f &= T_2 h - \Delta T \left[ \frac{\chi}{2V} - \frac{h}{e^{2Vh/\chi}} \right] \\ &\quad - \left( T_2 h - \Delta T \left[ \frac{\chi}{2V} - \frac{h}{e^{2Vh/\chi}} \right] \right) \\ &= \Delta T \left[ \frac{h}{e^{2Vh/\chi}} - \frac{h}{e^{-2Vh/\chi}} - 2 \frac{\chi}{2V} \right] \end{aligned}$$

$$= \Delta T \left[ \frac{h}{e^{2Vh/x} - 1} + \frac{h e^{2Vh/x}}{e^{2Vh/x} - 1} - 2 \frac{x}{2V} \right] \quad ||$$

$$= \Delta T \left[ h \frac{e^{2Vh/x} + 1}{e^{2Vh/x} - 1} - \frac{x}{V} \right]$$

$$= \Delta T \left[ h \coth \frac{Vh}{x} - \frac{x}{V} \right]$$

check:

$$f = \Delta T \cdot h \cdot \left[ \frac{x}{Vh} + \frac{1}{3} \frac{Vh}{x} + \dots - \frac{x}{Vh} \right]$$

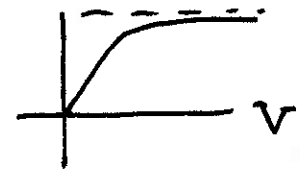
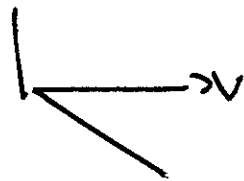
$$= \Delta T \cdot \frac{1}{3} \frac{Vh^2}{x} + \dots \quad \checkmark$$

so

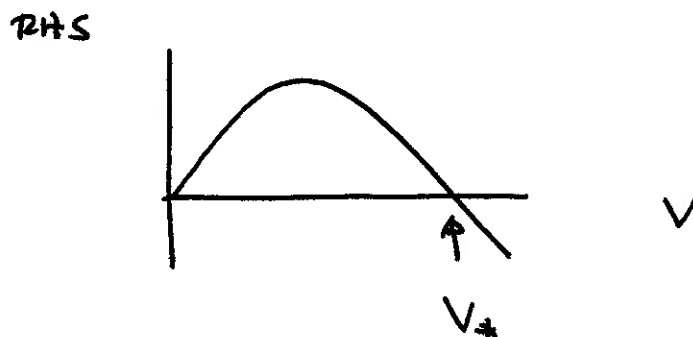
$$\frac{dV}{dt} = - \frac{8V}{a^2} V + \frac{g \alpha h}{2(l+w)} \Delta T \left[ \coth \frac{Vh}{x} - \frac{x}{Vh} \right]$$

$\frac{8V}{a^2} V$   
linear in  $V$

$\coth \frac{Vh}{x} - \frac{x}{Vh}$   
 $\rightarrow 1$  as  $V \rightarrow \infty$



Above threshold, the right-hand side has the form:



so  $V$  increases with time and asymptotically approaches  $V_*$  (constant velocity).

For  $\Delta T$  very large, the right-hand side is approximately

$$-\frac{8\nu}{a^2} V + \frac{g\alpha h}{2(h+w)} \Delta T \approx 1$$

and so

$$V_* = \frac{g\alpha a^2 h}{16\nu(h+w)} \Delta T$$

for large  $\Delta T$ .