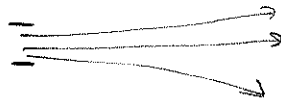


Physics 211 - Problem Set #6

Solutions

1.) a.)

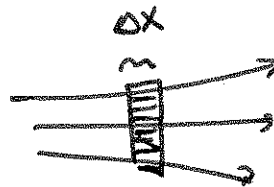


The fluid momentum density is

$$P_x = \rho v_x$$

At position x , the fluid emitted in an interval Δt occupies a slice of width

$$\Delta x = v_x \Delta t$$



The momentum in this slice is

$$\int dx dy \rho v_x = \int_{-\infty}^{\infty} dy \rho v_x^2 \Delta t = F \Delta t$$

per unit length in z . Viscosity transfers momentum laterally, from one value of y to another, so this quantity is conserved in the flow.

b.) In terms of the stream function ψ

$$v_x = \frac{\partial \psi}{\partial y} \quad v_y = -\frac{\partial \psi}{\partial x}$$

so

$$v_x \frac{\partial}{\partial x} v_x + v_y \frac{\partial}{\partial y} v_x = \nu \frac{\partial^2}{\partial y^2} v_x$$

become

$$\psi_y \psi_{xy} - \psi_x \psi_{yy} = \nu \psi_{yyy}$$

subscript = derivative

Look for a scaling solution

$$\psi = A x^p f(\eta) \quad \eta = \frac{y}{x^q}$$

$$\begin{aligned} \psi_y &= A x^{p-q} f'(\eta) & \psi_x &= A (p x^{p-1} f - q x^{p-1} \frac{y}{x^q} f') \\ & & &= A x^{p-1} (p f - q \eta f') \end{aligned}$$

so

$$\psi_y \psi_{xy} \sim x^{2p-2q-1}$$

$$\psi_x \psi_{yy} \sim x^{2p-2q-1}$$

$$\psi_{yyy} \sim x^{p-3q}$$

so for a scaling solution $2p-2q-1 = p-3q$

$$a \quad p+q=1$$

We need one more equation between p and q

This comes from the consistency of F :

$$F/\rho = \int dy v_x^2 = \int dy (\psi_y)^2 = \int d\eta x^q x^{2p-2q} (A f'(\eta))^2$$

$$\text{so } 2p - q = 0$$

$$\text{so } p = \frac{1}{3} \quad q = \frac{2}{3}$$

e.) Then $\psi_y \psi_{xy} - \psi_x \psi_{yy} = \nu \psi_{yyy}$ becomes

$$(A x^{-1/3} f') A x^{-2/3-2/3} \left(\frac{1}{3} f' - \frac{2}{3} f' - \frac{2}{3} \eta f'' \right)$$

$$- A x^{-2/3} \left(\frac{1}{3} f - \frac{2}{3} \eta f' \right) A x^{-1/3-2/3} f''$$

$$= \nu A x^{1/3-2} f''' = 0$$

or

$$A^2 \left[-\frac{1}{3} (f')^2 - \frac{2}{3} \eta f' f'' - \frac{1}{3} f f'' + \frac{2}{3} \eta f' f'' \right]$$

$$- \nu A^2 f''' = 0$$

set $\nu A = 6\nu$ to simplify this

$$f''' + 2 f f'' + 2 (f')^2 = 0$$

d.) Try

$$f = B \tanh \alpha \eta$$

$$f' = B \alpha \frac{1}{\cosh^2 \alpha \eta}$$

$$f'' = -2B \alpha^2 \frac{\sinh \alpha \eta}{\cosh^3 \alpha \eta}$$

$$\begin{aligned} f''' &= -2B \alpha^3 \left[\frac{\cosh \alpha \eta}{\cosh^3 \alpha \eta} - 3 \frac{\sinh^2 \alpha \eta}{\cosh^4 \alpha \eta} \right] \\ &= -2B \alpha^3 \left[\frac{\cosh^2 \alpha \eta - \sinh^2 \alpha \eta}{\cosh^4 \alpha \eta} - 2 \frac{\sinh^2 \alpha \eta}{\cosh^4 \alpha \eta} \right] \end{aligned}$$

$$f f'' + (f')^2 = + B^2 \alpha^2 \left[\frac{1}{\cosh^4 \alpha \eta} - 2 \frac{\sinh^2 \alpha \eta}{\cosh^4 \alpha \eta} \right]$$

so

$$f''' = (-2) [f f'' + (f')^2] \quad \text{if } B = \alpha$$

so $f = \alpha \tanh \alpha \eta$ for some α .

$$\begin{aligned} e.) \quad F/\rho &= \int_{-\infty}^{\infty} dy \, v_x^2 = A^2 \int_{-\infty}^{\infty} d\eta \left(\frac{\alpha^2}{\cosh^2 \alpha \eta} \right)^2 \\ &= 36v^2 \alpha^3 \int_{-\infty}^{\infty} d\omega \frac{1}{\cosh^4 \omega} \end{aligned}$$

Now we just need to evaluate the integral.

$$\cosh w = \frac{1}{2}(e^w + e^{-w}) = \frac{1}{2} e^{-w} (e^{2w} + 1)$$

$$I = \int_{-\infty}^{\infty} \frac{dw}{\cosh^4 w} = \int dw \ 16 e^{4w} \frac{1}{(e^{2w} + 1)^4}$$

$$\text{let } z = \frac{e^{2w}}{e^{2w} + 1} \quad (1-z) = \frac{1}{e^{2w} + 1}$$

$$-dz = -2dw \frac{e^{2w}}{(e^{2w} + 1)^2} = -2dw \ z(1-z)$$

$$I = 8 \int_0^1 \frac{dz}{z(1-z)} z^2(1-z)^2 = 8 \int_0^1 dz \ z(1-z) = \frac{8}{6} = \frac{4}{3}$$

$$\text{so } F/\rho = 48 v^2 \alpha^3$$

$$\alpha = \left[\frac{F}{48 v^2 \rho} \right]^{\frac{1}{3}} \quad \alpha x = \left[\frac{F}{48 \rho v^2 x^2} \right]^{\frac{1}{3}} y$$

$$\text{check units } \frac{F}{\rho} = \frac{[\text{gm/sec}] / \text{cm sec}}{\text{g/cm}^3} \sim \text{cm}^3 / \text{sec}^2$$

$$vx = \text{cm}^2 / \text{sec} \cdot \text{cm} \sim \text{cm}^3 / \text{sec}$$

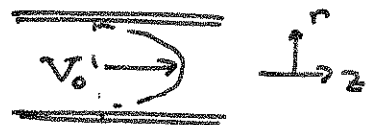
$$\text{so } \left[\frac{F}{\rho(vx)^2} \right]^{\frac{1}{3}} \sim \left[\frac{\text{cm}^3 / \text{sec}^2}{\text{cm}^6 / \text{sec}^2} \right]^{\frac{1}{3}} \sim \frac{1}{\text{cm}} \quad \checkmark$$

finally:

$$v_x = \left[\frac{3}{24} \frac{F^2}{\rho^2 v^4} \frac{1}{x} \right]^{\frac{1}{3}} \quad \frac{1}{\cosh^2 \left[\left[\frac{F}{48 \rho v^2 x^2} \right]^{\frac{1}{3}} y \right]}$$

2.) a.) In the pipe

$$v_z = V_0 \left(1 - \frac{r^2}{a^2}\right)$$



the source term for heat is

$$\begin{aligned} \frac{\nu}{2c_p} \left(\frac{\partial v_i^i}{\partial x^j} + \frac{\partial v_j^j}{\partial x^i} \right)^2 &= 2 \frac{\nu}{2c_p} \left(\frac{\partial v_z}{\partial r} \right)^2 \\ &\quad \uparrow \\ &\quad (\sigma^{rz})^2 \text{ and } (\sigma^{rz})^2 \text{ contribute} \\ &= \frac{\nu}{c_p} \left(-2V_0 \frac{r}{a^2} \right)^2 = \frac{4\nu V_0^2}{c_p} \frac{r^2}{a^4} \end{aligned}$$

b.) In the steady state, T is a function of r only

$$\text{so } \frac{\partial T}{\partial t} = 0 \quad \vec{\nabla} \cdot \vec{\nabla} T = 0$$

then

$$0 = \chi \nabla^2 T + \frac{4\nu V_0^2}{c_p} \frac{r^2}{a^4}$$

$$\frac{1}{r} \frac{d}{dr} r \frac{d}{dr} T(r) = - \frac{4\nu V_0^2}{\chi c_p} \frac{r^2}{a^4}$$

$$r \frac{d}{dr} T(r) = A - \frac{2\nu V_0^2}{\chi c_p} \frac{r^4}{a^4}$$

$$A \neq 0 \Rightarrow T(r) \sim \log r \text{ as } r \rightarrow 0 \text{ so } A = 0$$

then

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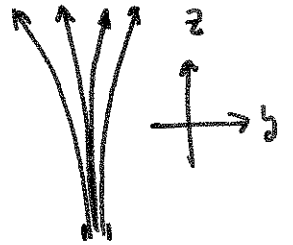
$$T(r) = C - \frac{\nu V_0^2}{4\lambda C_p} \frac{r^4}{a^4}$$

$$T(r) = T_0 \quad \text{at } r = a \quad \text{so}$$

$$T(r) = T_0 + \frac{\nu V_0^2}{4\lambda C_p} \left(1 - \frac{r^4}{a^4}\right)$$

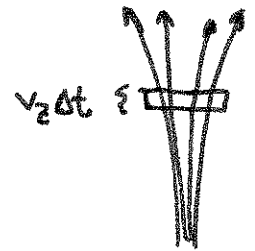
3.) a) In this problem, heat diffuses laterally as the fluid elements rise.

The heat in each horizontal slice is constant.



The density of heat is $\rho C_p \cdot \Delta T$

The heat in a slice emitted in Δt per unit length is:



$$\begin{aligned} Q \Delta t &= \int dy dz \rho C_p \Delta T \\ &= \rho C_p \left(\int_{-\infty}^{\infty} dy v_2 \Delta T \right) \Delta t \end{aligned}$$

$$Q = \rho C_p \int_{-\infty}^{\infty} dy v_2 \Delta T$$

b.) Under the assumptions of the problem

$$P = P_0 - \rho_0 g z$$

and in the plane $\rho = \rho_0 (1 - \alpha \Delta T)$

so there is a buoyancy force / cm³

$$f = \alpha \rho_0 g \Delta T \quad \text{upward}$$

$$\rho \frac{D V_z}{D t} = \rho V_z \frac{\partial}{\partial z} V_z = \alpha \rho_0 g \Delta T$$

then
$$\frac{\partial}{\partial z} \left(\frac{1}{2} V_z^2 \right) = \alpha g \Delta T$$

c.)
$$\frac{D}{D t} \delta^2 = V_z \frac{\partial}{\partial z} \delta^2 = \chi$$

Now assume

$$V_z = A z^\alpha \quad \Delta T = B z^\beta \quad \delta = C z^\gamma$$

Determine α, β, γ :

$$\delta \cdot V_z \cdot \Delta T \sim 1 \quad \Rightarrow \quad z^{\alpha + \beta + \gamma} \sim 1$$

$$\frac{\partial}{\partial z} (V_z^2) \sim \Delta T \quad \Rightarrow \quad z^{2\alpha - 1} \sim z^\beta$$

$$V_z \frac{\partial}{\partial z} \delta^2 \sim 1 \quad \Rightarrow \quad z^{\alpha + 2\gamma - 1} \sim 1$$

$$\text{so } \begin{cases} \alpha + \beta + \gamma = 0 \\ \alpha + 2\gamma = 1 \\ 2\alpha - \beta = 1 \end{cases} \rightarrow \alpha = \frac{1}{5} \quad \beta = -\frac{3}{5} \quad \gamma = \frac{2}{5}$$

$$\text{so } \delta \sim z^{2/5}$$

d.) Finally, determine A, B, C

$$\frac{Q}{\rho c_p} = ABC$$

$$\frac{\partial}{\partial z} \left(\frac{1}{2} V_z^2 \right) = A^2 z^{-3/5} = \alpha g B z^{-3/5}$$

$$V_z \frac{\partial}{\partial z} \delta^2 = AC^2 = \chi$$

$$\sqrt{ABC} = A^{5/2} \frac{\chi^{1/2}}{\alpha g} = \frac{Q}{\rho c_p}$$

$$\text{so } A = \left(\frac{Q}{\rho c_p} \cdot \alpha g \right)^{2/5} \chi^{-1/5} \quad B = \left(\frac{Q}{\rho c_p} \right)^{4/5} (\alpha g)^{-1/5} \chi^{-2/5}$$

$$C = \left(\frac{Q}{\rho c_p} \right)^{-1/5} (\alpha g)^{-1/5} \chi^{3/5}$$

$$\text{thus: } V_z = \left(\frac{Q}{\rho c_p} \right)^{2/5} (\alpha g)^{2/5} \chi^{-1/5} z^{1/5}$$

$$\Delta T = \left(\frac{Q}{\rho c_p} \right)^{4/5} (\alpha g)^{-1/5} \chi^{-1/5} z^{-3/5}$$

$$\delta = \left(\frac{Q}{\rho c_p} \right)^{-1/5} (\alpha g)^{-1/5} \chi^{3/5} z^{2/5}$$

e.) Now redo the analysis for a point source

$$Q = \text{heat/sec} = \rho c_p \int dx_1 v_z \Delta T \sim \rho c_p \delta^2 v_z \Delta T$$

and, still: $\frac{\partial}{\partial z} (\frac{1}{2} v_z^2) = \alpha g \Delta T$

$$v_z \frac{\partial}{\partial z} \delta^2 = \chi$$

so if we assume the power law forms on p. 8

$$\left. \begin{aligned} \alpha + \beta + 2\gamma &= 0 \\ \alpha + 2\gamma &= 1 \\ 2\alpha - \beta &= 1 \end{aligned} \right\} \alpha = 0 \quad \beta = 1 \quad \gamma = \frac{1}{2}$$

$$\frac{Q}{\rho c_p} = ABC^2 \quad A^2 = \alpha g B$$

$$\hookrightarrow AC^2 = \chi$$

$$\text{then } ABC^2 = \chi B = \frac{Q}{\rho c_p}$$

$$B = \frac{Q}{\rho c_p} \frac{1}{\chi}$$

$$A = \left(\frac{Q}{\rho c_p} \right)^{1/2} (\alpha g)^{1/2} \chi^{-1/2}$$

$$C = \left(\frac{Q}{\rho c_p} \right)^{-1/4} (\alpha g)^{-1/4} \chi^{3/4}$$

then

$$V_z = \left(\frac{Q}{\rho c_p}\right)^{1/2} (\alpha g)^{1/2} \chi^{-1/2} \quad \text{indep. of } z$$

$$\Delta T = \frac{Q}{\rho c_p} \frac{1}{\chi} \frac{1}{z}$$

$$\delta = \left(\frac{Q}{\rho c_p}\right)^{-1/4} (\alpha g)^{-1/4} \chi^{3/4} z^{1/2}$$