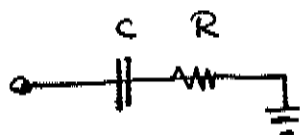


# the Fourier Transform

Jan 17

In the previous lecture, we analyzed circuits driven by AC voltage oscillating at a fixed frequency. For example: if

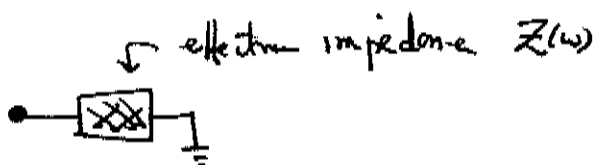


is driven by  $V(t) = V_0 \cos \omega t = \operatorname{Re} V_0 e^{-i\omega t}$

the current that flows in response is

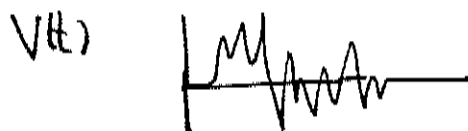
$$I(t) = \operatorname{Re} I_0 e^{-i\omega t} \quad \text{with} \quad I_0 = \frac{V_0}{R + i/\omega C}$$

in general



$$I_0 = \frac{V_0}{Z(\omega)}$$

Now, what happens if we drive the circuit with a signal which is a more arbitrary function of time?



There are two aspects to the problem. First, if the behavior of the circuit is described by a differential equation, we might

with the find a solution of the differential equation with  
source term  $V(t)$ . In the case of the simple circuit above

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$$V(t) = R \frac{dQ}{dt} + \frac{1}{C} Q$$

The most general solution to this differential equation is

$$Q(t) = Q_p(t) + Q_0(t)$$

where  $Q_p(t)$  is a particular solution to the inhomogeneous  
equation and  $Q_0(t)$  is a general solution to the equation with  $V(t) = 0$ .

For this equation,

$$Q_0(t) = a e^{-t/RC}$$

where  $a$  is a constant, so the second term falls off in a natural  
damping time for the circuit. This term is called a "transient".

Let's first discuss how to compute the particular solution  
 $Q_p(t)$ , then come back and solve for the transient behavior.

Since we know how to find  $Q_p(t)$  when  $V(t)$  is an  
oscillator with a definite frequency, let's try to reduce  
the whole to a general  $V(t)$  to this case. If  $V(t)$  is  
periodic with period  $T$ , we can represent  $V(t)$  by  
a Fourier series

$$V(t) = \sum_{n=-\infty}^{\infty} V_n e^{-i 2\pi n t / T}$$

The coefficients in this series are calculated by

the formula

$$V_n = \frac{1}{T} \int_0^T V(t) e^{i 2\pi n t / T} dt$$

There is a nice consistency check:

$$V_n \stackrel{?}{=} \frac{1}{T} \int_0^T e^{i 2\pi n t / T} \sum_{m=-\infty}^{\infty} V_m e^{-i 2\pi m t / T} dt$$

By the orthogonality of sin's and cos's, the integral vanishes unless  $n=m$ ; in that case, the integral is trivial. So

$$\frac{1}{T} \int_0^T e^{i 2\pi n t / T} e^{-i 2\pi m t / T} dt = \delta_{nm}$$

and the check succeeds. In the other direction, we should have

$$V(t) = \sum_{n=-\infty}^{\infty} e^{-2\pi i n t / T} \frac{1}{T} \int_0^T e^{2\pi i n t' / T} V(t') dt'$$

$$= \int_0^T dt' \left\{ \frac{1}{T} \sum_{n=-\infty}^{\infty} e^{-2\pi i n t / T} e^{2\pi i n t' / T} \right\} V(t')$$

which is consistent if

$$\frac{1}{T} \sum_{n=-\infty}^{\infty} e^{-2\pi i n t / T} e^{2\pi i n t' / T} = \delta(t-t')$$

All of these formula apply if  $V(t)$  is complex. If  $V(t)$  is real, the Fourier series coefficients are restricted by

$$V_{-n} = (V_n)^*$$

What if the signal  $V(t)$  is not periodic? We can always view it as being periodic with a very large period. So let's try to take the limit  $T \rightarrow \infty$  of the formulae above and see if we get a sensible result.

Let

$$\omega = \frac{2\pi n}{T} \quad \text{so} \quad e^{-2\pi i n t / T} \rightarrow e^{-i \omega t}$$

for finite  $T$ , the  $\omega$  are discrete multiples of  $\frac{2\pi}{T}$ . As  $T \rightarrow \infty$ , these frequencies become continuous. Then

$$\sum_{n=-\infty}^{\infty} \approx \int_{-\infty}^{\infty} dn \rightarrow \frac{T}{2\pi} \int_{-\infty}^{\infty} d\omega$$

$$\text{so} \quad \frac{1}{T} \sum_{n=-\infty}^{\infty} \rightarrow \int_{-\infty}^{\infty} \frac{d\omega}{2\pi}$$

$$\text{Let} \quad \tilde{V}(\omega) = T V_n$$

Then the formulae above go over to

$$V(t) = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} \tilde{V}(\omega) e^{-i\omega t}$$

$$\tilde{V}(\omega) = \int_{-\infty}^{\infty} dt V(t) e^{i\omega t}$$

These formulae are consistent if

$$V(t) = \int \frac{d\omega}{2\pi} e^{-i\omega t} \int dt' e^{i\omega t'} V(t')$$

is. if

$$\int \frac{d\omega}{2\pi} e^{-i\omega(t-t')} = \delta(t-t')$$

and if

$$\tilde{V}(\omega) = \int dt e^{i\omega t} \left( \int \frac{d\omega'}{2\pi} e^{-i\omega' t} \tilde{V}(\omega') \right)$$

is. if

$$\int dt e^{i(\omega-\omega')t} = 2\pi \delta(\omega-\omega')$$

The first of these formulae is the  $T \rightarrow \infty$  limit of the formula at the bottom of p.3. The  $T \rightarrow \infty$  limit of the formula is the middle of p.3

$$\int_0^T dt e^{i \frac{2\pi n}{T} t} e^{-i \frac{2\pi m}{T} t} = T \delta_{nm} = 2\pi \frac{T}{2\pi} \delta_{nm}$$

indeed gives the second formula above when we realize that  $2\pi/T = \Delta\omega$ , the spacing of the discrete  $\omega$ 's. Then

$$\frac{1}{\Delta\omega} \delta_{nm} \rightarrow \delta(\omega-\omega')$$

The function  $\tilde{V}(\omega)$  represents the decomposition of the function  $V(t)$  into components of definite frequency.  $\tilde{V}(\omega)$  is called the Fourier transform of  $V(t)$ . Given the simple inversion formulae,  $V(t)$  and  $\tilde{V}(\omega)$  are two equivalent representations of the same information,  $V(t)$  in time and  $\tilde{V}(\omega)$  in frequency space. If  $V(t)$  is real-valued,  $\tilde{V}(\omega)$  obeys the

"reality condition"  $\tilde{V}(-\omega) = [\tilde{V}(\omega)]^*$

Notice that the inversion formulas and also the integrals which give  $\delta$ -functions, contain factors of  $2\pi$  asymmetrically. Some people like to move around factors of  $\sqrt{2\pi}$  to make the formulas symmetrical. In my experience, you will drop ~~many~~ fewer factors of  $2\pi$  if you just make it a habit to write the  $2\pi$  with  $\omega$ :

$$\int \frac{d\omega}{2\pi} \quad 2\pi \delta(\omega - \omega')$$

Given the Fourier transform of a signal  $V(t)$ , we can find a solution for the current in any circuit. The response to

$$V(t) = \text{Re } \tilde{V}(\omega) e^{-i\omega t} \quad \text{is} \quad I(t) = \text{Re } \frac{\tilde{V}(\omega)}{Z(\omega)} e^{-i\omega t}$$

Then, by superposition, a general  $V(t)$  yields

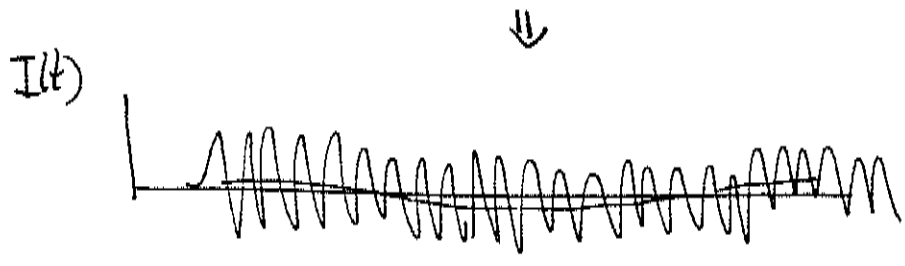
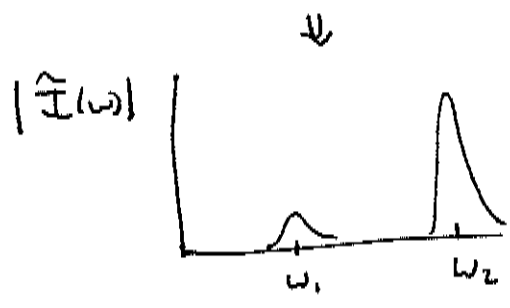
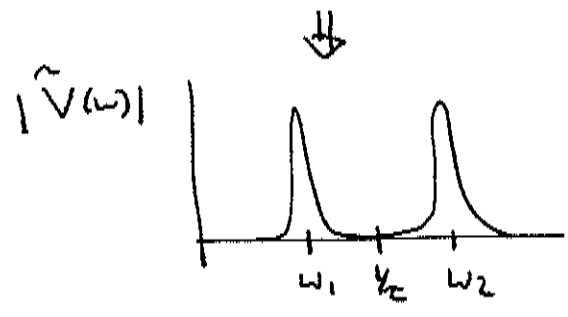
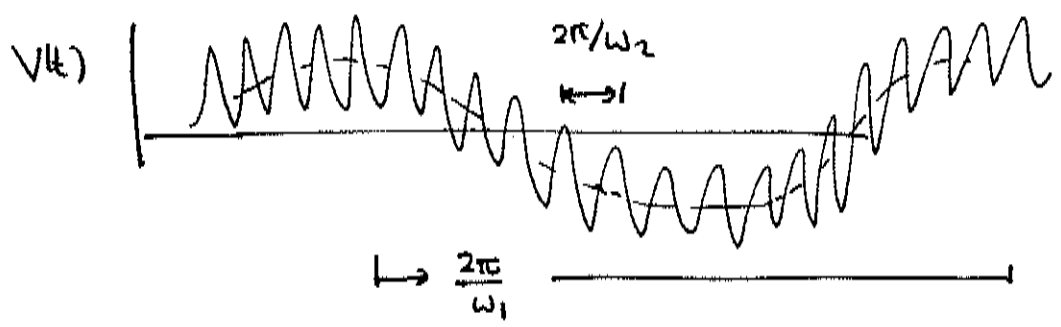
$$I(t) = \int \frac{d\omega}{2\pi} \frac{\tilde{V}(\omega)}{Z(\omega)} e^{-i\omega t}$$

When we looked at particular circuits, we saw that they could have a different ~~response~~ response for different frequencies. For example, the single circuit on p. 1

has 
$$\frac{1}{Z(\omega)} = \frac{1}{R + i/\omega C} = \frac{\omega C}{\omega CR + i}$$

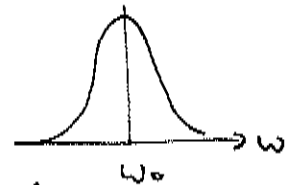
$$\left| \frac{1}{Z(\omega)} \right| = \frac{\omega C}{[(\omega CR)^2 + 1]^{\frac{1}{2}}}$$

For  $\omega \gg \frac{1}{RC}$   $\tau = RC$ ,  $\frac{1}{Z} \approx \frac{1}{R}$  and the circuit feels no effect of the capacitor. For  $\omega \ll \frac{1}{RC}$ , the capacitor essentially stops the flow of current and so the response is very small. Essentially, this  $Z(\omega)$  allows the high frequency components of the signal to pass while damping out the low frequencies. Here is a graphical illustration of this process



It is very useful to learn to think in frequency space, to visualize the decomposition of a given waveform in terms of frequencies and the waveform that results when this frequency spectrum is modified in some way. A useful tool to help this process of visualization is the "Gaussian wavepacket."

$$\tilde{f}(\omega) = e^{-a^2(\omega-\omega_0)^2/2}$$



This is a concentrated set of frequencies, centered on  $\omega_0$ , with width  $\Delta\omega \approx 1/a$ . Going back to "real space" by inverting the Fourier transform, we find

$$f(t) = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} e^{-a^2(\omega-\omega_0)^2/2} e^{-i\omega t}$$

$$= \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} e^{-i\omega_0 t} e^{-\frac{a^2}{2}(\omega-\omega_0)^2 - i(\omega-\omega_0)t}$$

write the exponent  
as a perfect square

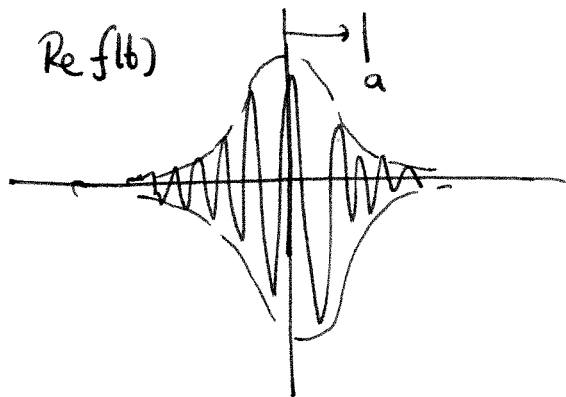
$$= \int_{-\infty}^{\infty} \frac{d(\omega-\omega_0)}{2\pi} e^{-i\omega_0 t} e^{-\frac{a^2}{2}(\omega-\omega_0 + i\frac{t}{a^2})^2} e^{-t^2/2a^2}$$

now use  $\int_{-\infty}^{\infty} dx e^{-x^2} = \sqrt{\pi} \Rightarrow \int_{-\infty}^{\infty} \frac{dx}{\pi} e^{-\frac{a^2}{2}x^2} = \frac{1}{\sqrt{2\pi a^2}}$

to complete the integral!

$$f(t) = \frac{1}{\sqrt{2\pi a^2}} e^{-i\omega_0 t} e^{-t^2/2a^2}$$

so this is a "packet", centered on  $t=0$ , of width  $\Delta t = a$ , containing an oscillation at  $\omega_0$



Following the same analysis with the wavepacket

$$\tilde{f}_{t_0}(\omega) = e^{-a^2(\omega-\omega_0)^2/2} e^{i\omega t_0}$$

we find that the real space form is

$$\int \frac{d\omega}{2\pi} \tilde{f}_{t_0}(\omega) e^{-i\omega t} = f(t-t_0)$$

the Gaussian wavepacket of width  $a$  centered at  $t=t_0$ .  
By dividing a real-space signal into wavepackets, we can see how it translates into a shape in frequency space.

Let's look once more at the formula for  $I(t)$  on p. 6 and find another interpretation of this formula. Start with

$$I(t) = \int \frac{d\omega}{2\pi} \frac{\tilde{V}(\omega)}{Z(\omega)} e^{-i\omega t}$$

and introduce the inverse transform

$$\tilde{V}(\omega) = \int dt V(t) e^{i\omega t}$$

$$\frac{1}{Z(\omega)} = \int dt Z(t) e^{i\omega t}$$

then

$$I(t) = \int \frac{d\omega}{2\pi} \int dt_1 V(t_1) \int dt_2 Z(t_2) e^{i\omega(t_1+t_2-t)}$$

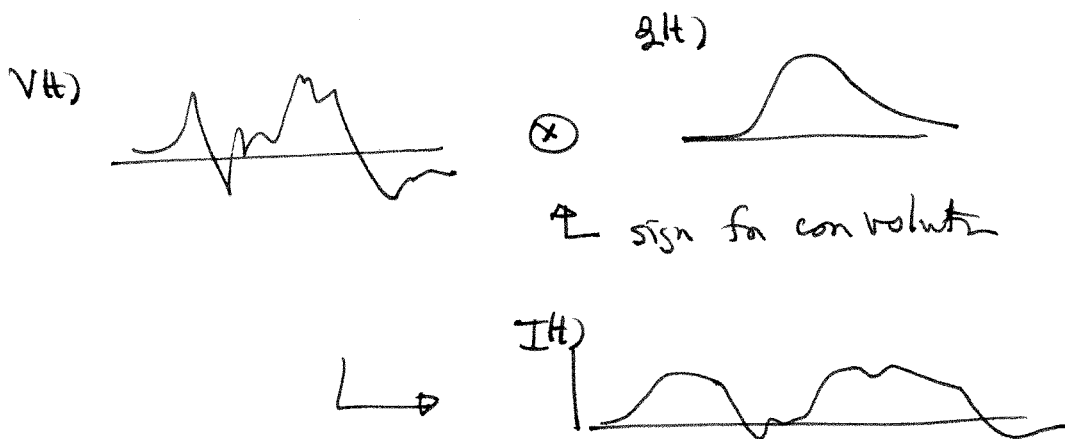
$$= \int dt_1 dt_2 Z(t_2) V(t_1) \delta(t_1+t_2-t)$$

we can use the  $\delta$ -function to do the  $t_2$  integral and obtain:

$$I(t) = \int dt_1 Z(t-t_1) V(t_1)$$

This structure is called a "convolution". The signal  $V(t_1)$  is smeared out by the response of the circuit, encoded as  $Z(t)$ . This function is, well, whatever has the Fourier transform  $\frac{1}{Z(\omega)}$ . Roughly, the convolution process

looks like



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The result we have just derived is a special case of the "convolution theorem":

Given functions  $f(t)$ ,  $g(t)$  with Fourier transforms  $\hat{f}(\omega)$ ,  $\hat{g}(\omega)$  the function with Fourier transform  $\hat{f}(\omega) \cdot \hat{g}(\omega)$  is

$$F(t) = f \otimes g(t) = \int_{-\infty}^{\infty} dt' f(t-t') g(t')$$

"the convolution of  $f$  with  $g$ ".

Very typically, the response of a linear device is the convolution of the original signal with a "response function" ( $g(t)$  in the example above).