

$$1.) \quad i) \nabla \cdot \mathbf{E} = 0$$

$$ii) \nabla \cdot \mathbf{B} = 0$$

$$iii) \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$iv) \nabla \times \mathbf{B} = \frac{\partial \mathbf{E}}{\partial t}$$

$$\frac{\partial}{\partial t} \text{ of } iv) \Rightarrow \frac{\partial^2 \mathbf{E}}{\partial t^2} = \nabla \times \frac{\partial \mathbf{B}}{\partial t}$$

$$\text{use } iii) \Rightarrow \frac{\partial^2 \mathbf{E}}{\partial t^2} = -\nabla \times (\nabla \times \mathbf{E})$$

$$\frac{\partial^2 \mathbf{E}}{\partial t^2} = -\nabla \times \nabla \times \mathbf{E} = -(\nabla(\nabla \cdot \mathbf{E}) - \nabla^2 \mathbf{E})$$

$$\text{use } i) \Rightarrow \nabla^2 \mathbf{E} = \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

$$\nabla^2 \mathbf{E} = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \mathbf{E}}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \mathbf{E}}{\partial \varphi^2} + \frac{\partial^2 \mathbf{E}}{\partial z^2} = \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

take z-component & use ansatz $E_z = E_0 f(r) e^{i(\omega t - kz)}$

$$\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 f') - k^2 f = -\omega^2 f$$

$$f'' + \frac{1}{r} f' + (\omega^2 - k^2) f = 0$$

This satisfies Bessel's Eqn. for $J_0 (n=0)$ if $\omega^2 - k^2 = 1$

We thus get $f(r) = J_0(r)$ w/ our dispersion relation

$$\omega = \pm \sqrt{1 + k^2}$$

But we need $E_z = 0$ at the boundary so we need to scale our soln st we find $f(R) = 0$. We will use the fact that $J_0(2.405...) = 0$

Let $u = \alpha r$, Let $g(u) = g(\alpha r) = f(r)$

$$g' = \frac{dg}{du} = \frac{dg(u)}{du} = \frac{dg(\alpha r)}{du} = \frac{dg(\alpha r)}{dr} \frac{du}{dr} = \frac{df}{dr} \frac{du}{dr} = \alpha f'$$

Similarly, $g'' = \alpha^2 f''$

$$\alpha^2 g'' + \frac{\alpha}{u} g' + (\omega^2 - k^2) g = 0$$

$$g'' + \frac{1}{u} g' + \left(\frac{\omega^2 - k^2}{\alpha^2} \right) g = 0$$

$$\Rightarrow g(u) = J_0(u), f(r) = J_0(\alpha r), f(R) = 0 \Rightarrow \alpha R \approx 2.405 \Rightarrow \alpha \approx \frac{2.405}{R}$$

$$f(r) = J_0(2.405 r/R) \quad \& \quad \frac{\omega^2 - k^2}{\alpha^2} = 1 \Rightarrow \omega = \pm \sqrt{\left(\frac{2.405}{R} \right)^2 + k^2}$$

$$f(r) = J_0\left(\frac{u_{01} r}{R}\right)$$

$$\omega = \pm \sqrt{\left(\frac{u_{01}}{R}\right)^2 + k^2}$$

$$u_{01} \approx 2.405, \quad J_0(u_{01}) = 0$$

$$\omega^2 - k^2 = \frac{u_{01}^2}{R^2}, \quad \frac{\omega^2}{k^2} - 1 = \frac{u_{01}^2}{k^2 R^2} = \frac{u_{01}^2}{R^2} \frac{1}{\omega^2 - \frac{u_{01}^2}{R^2}} = \frac{u_{01}^2}{R^2 \omega^2 - u_{01}^2}$$

$$\frac{\omega^2}{k^2} = 1 + \frac{u_{01}^2}{R^2 \omega^2 - u_{01}^2} = \frac{R^2 \omega^2}{R^2 \omega^2 - u_{01}^2}$$

$$V_p(\omega) = \frac{\omega}{k} = \left(\frac{R^2 \omega^2}{R^2 \omega^2 - u_{01}^2}\right)^{1/2}$$

$$R^2 \omega^2 > R^2 \omega^2 - u_{01}^2 \Rightarrow V_p(\omega) > 1 \quad \forall \omega \quad (\text{provided } V_p \text{ is real, or } R^2 \omega^2 - u_{01}^2 > 0)$$

($\omega > \frac{u_{01}}{R}$)

minimum ω_c is given as $k \rightarrow 0$
(or as $V_p \rightarrow \text{imaginary}$)

$$\omega_c = \frac{u_{01}}{R} \approx \frac{2.405}{R}$$

$$\text{if } R = 5 \text{ cm, } v_c = \frac{\omega_c}{2\pi} = \frac{u_{01}}{2\pi R} = \frac{2.405}{2\pi \cdot 5 \text{ cm}} \approx 0.077 \text{ cm}^{-1}$$

$$\approx 2.30 \text{ GHz}$$

2.)

$$p_1 = (E_1, \vec{p}_1) = E_1(1, 1)$$

$$p_2 = E_2(1, -1)$$

$$p_{\text{tot}} = (E_1 + E_2, E_1 - E_2)$$

$$p_{\text{tot}}^2 = (E_1 + E_2)^2 - (E_1 - E_2)^2 = 4E_1 E_2 = E_{\text{cm}}^2$$

$$E_1 = 9 \text{ GeV}$$

$$E_{\text{cm}} = 10.56 \text{ GeV}$$

$$E_2 = \frac{E_{\text{cm}}^2}{4E_1} = \boxed{3.098 \text{ GeV}}$$

$$\text{current} = \frac{\#e^-}{\text{dist}} \cdot \text{speed} \cdot \frac{C}{e^-}$$

speed = c for both beams (bc 9.3 GeV \gg 5 meV)

$$\text{HER: } I = \frac{1658 \cdot 2.7 \cdot 10^{10} e^-}{2200 \text{ m}} \cdot 2.998 \cdot 10^8 \frac{\text{m}}{\text{s}} \cdot \frac{1.602 \cdot 10^{-19} \text{ C}}{e^-} \approx 9.773 \text{ C/s} \approx \boxed{.98 \text{ amper}}$$

$$\text{LER: } I = \frac{1658 \cdot 5.9 \cdot 10^{10} e^-}{2200 \text{ m}} \cdot 2.998 \cdot 10^8 \frac{\text{m}}{\text{s}} \cdot \frac{1.6 \cdot 10^{-19} \text{ C}}{e^-} \approx \boxed{2.1 \text{ amper}}$$

$$\Delta E = \frac{4\pi\alpha}{3} \frac{E^4}{m^4/2}$$

$$\text{HER: } \Delta E = \frac{4\pi}{3} \frac{1}{137} \frac{(9 \text{ GeV})^4}{(5.11 \cdot 10^{-4} \text{ GeV})^4} \left(\frac{1}{2\pi} \right) \approx 8.4 \cdot 10^2 \text{ m}^{-1} \cdot (197 \text{ MeV} \cdot \text{fm}) \left(\frac{\text{m}}{10^5 \text{ fm}} \right) \approx \boxed{1.7 \text{ MeV}}$$

$$\text{LER: } \Delta E \approx \boxed{.023 \text{ MeV}}$$

$$P = \frac{\Delta E}{\Delta t} = (\Delta E) \left(\frac{\#e^-}{\text{s}} \right) \frac{2.998 \cdot 10^8 \text{ m/s}}{2200 \text{ m}}$$

$$\text{HER: } P = (1.7 \text{ MeV}) \left(1658 \cdot 2.7 \cdot 10^{10} \right) \left(\frac{2.998 \cdot 10^8 \text{ m/s}}{2200 \text{ m}} \right) \left(\frac{1.6 \cdot 10^{-13} \text{ A}}{\text{MeV}} \right) \approx \boxed{1.7 \cdot 10^6 \text{ W}}$$

$$\text{LER: } P \approx \boxed{4.9 \cdot 10^4 \text{ W}}$$

* see note on next page about bending

TeVatron

$$p^+ \text{ ring: } P \approx \frac{4\pi}{3} \frac{1}{137} \frac{(960 \text{ GeV})^4}{(938 \text{ GeV})^4} \left(\frac{1}{6300 \text{ m}} \right) \left(\frac{197}{10^5} \text{ MeV} \cdot \text{m} \right) \left(36 \cdot 2.7 \cdot 10^{11} \right) \left(\frac{3 \cdot 10^8 \text{ m/s}}{6300 \text{ m}} \right) \left(\frac{1.6 \cdot 10^{-13} \text{ A}}{\text{MeV}} \right)$$

$$\approx \boxed{.49 \text{ W}}$$

$$\text{if } e^-: P \approx \boxed{5.5 \cdot 10^{12} \text{ W}}$$

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Why would we want to lump the bending into short segments to increase the radiation?

Well, the LER is actually "too big" for its energy. Some synchrotron radiation is good in that it acts a little like focusing - it reduces the energy of the higher energy particles more than the lower energy.

Plus we can then also control where the radiation strikes the walls of the vacuum chamber. We can then make a cheaper ring b/c we need less ^{of the} special surface designed to absorb the radiation.

$$3.) M_x = \begin{pmatrix} \cos kl & k^{-1} \sin kl \\ -k \sin kl & \cos kl \end{pmatrix} \\ \approx \begin{pmatrix} 1 - \frac{(kl)^2}{2} & l \\ -k^2 l & 1 - \frac{(kl)^2}{2} \end{pmatrix} \approx \begin{pmatrix} 1 & l \\ -k^2 l & 1 \end{pmatrix}$$

$$M_c = \begin{pmatrix} 1 & \\ -\frac{1}{f} & 1 \end{pmatrix}, M_z = \begin{pmatrix} 1 & z \\ & 1 \end{pmatrix}$$

$$M_{z_1} M_c M_{z_2} = \begin{pmatrix} 1 & z_1 \\ & 1 \end{pmatrix} \begin{pmatrix} 1 & \\ -\frac{1}{f} & 1 \end{pmatrix} \begin{pmatrix} 1 & z_2 \\ & 1 \end{pmatrix} \approx \begin{pmatrix} 1 - z_1/f & z_1 + z_2 \\ -1/f & 1 - z_2/f \end{pmatrix}$$

$$f \approx \frac{1}{k^2 l}, z_1 \approx z_2 \approx \frac{l}{2}$$

$$M_y = \begin{pmatrix} \cos kl & k^{-1} \sin kl \\ k \sin kl & \cos kl \end{pmatrix} \approx \begin{pmatrix} 1 + \frac{(kl)^2}{2} & l \\ k^2 l & 1 + \frac{(kl)^2}{2} \end{pmatrix}$$

$$M_d = \begin{pmatrix} 1 & \\ \frac{1}{f} & 1 \end{pmatrix}, M_{z_3} M_d M_{z_4} \approx \begin{pmatrix} 1 + z_3/f & z_3 + z_4 \\ \frac{1}{f} & 1 + z_4/f \end{pmatrix}$$

$$f \approx \frac{1}{k^2 l}, z_3 \approx z_4 \approx \frac{l}{2}$$

$$M_d M_z M_c = \begin{pmatrix} 1 & z \\ \frac{1}{f} & 1 \end{pmatrix} \begin{pmatrix} 1 & z \\ & 1 \end{pmatrix} \begin{pmatrix} 1 & \\ -\frac{1}{f} & 1 \end{pmatrix} \approx \begin{pmatrix} 1 & z \\ -z/f^2 & 1 \end{pmatrix}$$

$$\Rightarrow \text{focusing w/ } -\frac{1}{f'} = -\frac{z}{f^2} \Rightarrow f' \approx f^2/z$$

$$M_c M_z M_d \approx \begin{pmatrix} 1 & z \\ -z/f^2 & 1 \end{pmatrix} \Rightarrow \text{again focusing w/ } \frac{1}{f'} \approx \frac{z}{f^2} \\ f' \approx f^2/z$$

4.) Griffiths 4.11

$$\Delta^{++} \Rightarrow p \pi^+$$

$$\text{int ang mom.} = \frac{3}{2} = \text{spin of } \Delta^{++} = J$$

$$\text{spin } p = \frac{1}{2}$$

$$\text{spin } \pi^+ = 0$$

$$\Rightarrow \text{total final spin ang. mom.} = \frac{1}{2} = S$$

$$L = J - S = \frac{3}{2} - \frac{1}{2} = 1 \text{ or } 2$$

5.) Griffiths 4.27

$$\mathbf{I} = \mathbf{I}_1 + \mathbf{I}_2$$

$$\mathbf{I}^2 = \mathbf{I}_1^2 + \mathbf{I}_2^2 + 2\mathbf{I}_1 \cdot \mathbf{I}_2$$

$$\mathbf{I}_1 \cdot \mathbf{I}_2 = \frac{1}{2}(\mathbf{I}^2 - \mathbf{I}_1^2 - \mathbf{I}_2^2)$$

$$\mathbf{I}_j^2 = \frac{j(j+1)}{4}$$

$$\mathbf{I}_1^2 = \frac{1}{2}(\frac{1}{2}+1) = \frac{3}{4} = \mathbf{I}_2^2$$

$$\text{in triplet } \mathbf{I}^2 = 1(1+1) = 2$$

$$\mathbf{I}_1 \cdot \mathbf{I}_2 = \frac{1}{2}(2 - 2 \cdot \frac{3}{4}) = \frac{1}{4}$$

$$\text{in singlet } \mathbf{I}^2 = 0(0+1) = 0$$

$$\mathbf{I}_1 \cdot \mathbf{I}_2 = -\frac{3}{4}$$

6.) Griffiths 4.32

Σ^{*0} is isospin $|1,0\rangle$

$$\Sigma^+ = |1,1\rangle = \pi^+$$

$$\Sigma^0 = |1,0\rangle = \pi^0$$

$$\Sigma^- = |1,-1\rangle = \pi^-$$

$$\Sigma^+ \pi^- = |1,1\rangle \otimes |1,-1\rangle = \frac{1}{\sqrt{6}} |2,0\rangle + \frac{1}{\sqrt{2}} |1,0\rangle + \frac{1}{\sqrt{3}} |0,0\rangle$$

$$\Sigma^0 \pi^0 = |1,0\rangle \otimes |1,0\rangle = \frac{\sqrt{2}}{3} |2,0\rangle + 0 |1,0\rangle + \frac{1}{\sqrt{3}} |0,0\rangle$$

$$\Sigma^- \pi^+ = |1,-1\rangle \otimes |1,1\rangle = \frac{1}{\sqrt{6}} |2,0\rangle + \frac{1}{\sqrt{2}} |1,0\rangle + \frac{1}{\sqrt{3}} |0,0\rangle$$

} from CG tables
for 1×1

branching ratio is proportional to square of coefficient of $|1,0\rangle$ (the isospin of Σ^{*0})

So to the extent in which isospin is a good symmetry,

half the Σ^{*0} decays go to $\Sigma^+ \pi^-$ and the other half to $\Sigma^- \pi^+$